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ABSTRACT This article describes the simulation method for layering the components of the charge in the blast furnace, including the particle size distribution and gas flow distribution of bell-less top charging systems in blast furnaces. The Burden Distribution application, which simulates the charge in blast furnaces operated by the company Třinecké železářny (ironworks) to optimize the production of pig iron, applied this simulation method. Based on the parabolic trajectory of the material falling from the tilting chute of the bell-less top charging system, the method is calculating the profile of individual charge layers. The material forms after impact according to known angles of repose, segregating into individual granulometric size fractions. The data incorporated into the simulation enables the estimation of charge and gas flow distribution along the radius of the blast furnace shaft. The article presents the used mathematical models and equations, including algorithms of the simulation. The profile of the individual blast furnace charge components determines the reducing gas flow distribution and thus the performance and energetic parameters of the operation of the blast furnace and consequently the production of pig iron. Technologists have therefore been striving to obtain information about gas flow and charge distribution. A bell-less top charging system is a useful tool for controlling both these flows. We can measure the effects of changes in the charging program, which consist of step-by-step changing the chute inclination during rotation both directly and indirectly. Indirect information includes temperature distribution on the perimeter of the charging system and in the gas pipelines, whereas profilometers can obtain direct information. Another option is to conduct mathematical simulations, which makes it possible to gain detailed information with minimal costs. This article focuses on a method for calculating a simulated model of the burden layer profile, including granulometric size distribution based on measurements of individual parameters and a simulation calculation. The well-researched parabolic falling trajectory of the burden leaving the chute of the bell-less top charging system is the basis of this model. The angle of the chute and the velocity of the burden leaving the tip of the chute to define the trajectory. After the material falls, it forms into a shape according to known angles of repose. The granular material segregates into the individual granulometric size fractions along the shaft radius of the blast furnace based on experimental estimation. The segregation of granular material means that larger pieces move further from the place of impact, while smaller pieces stay near the place of impact. An approximate differential equation describes granulometric segregation. Many experimenters explore the behaviour of gas flow through charges. There are even parameters available describing the dependence of pressure loss on the volume flow square for materials with known granulometric size spectra. All this data incorporates into the simulation calculation, which makes it possible to estimate the charge flow and gas distribution along the radius of the blast furnace stack. The model simulates the burden distribution on the radius of the blast furnace shaft. During charging, the chute of the bell-less top charging system rotates and gradually changes the angle of inclination α , so that the individual placements of iron ore or sinter, coke and additives like for example limestone could be checked along the shaft radius. In simple terms, we can assume that separate charges flow along the falling trajectory (Figure 1). The velocity of the burden into the chute and the chute angle determine the material falling trajectory. Equation (1) describes the velocity of the burden at the tip of the chute calculation [1]. (1) $v_1 = v_0 \cos 2(\alpha) + \omega L 2 \sin(\alpha)(\sin \alpha + \mu \cos \alpha) + 2g L (\cos \alpha - \mu \sin \alpha) / 2(1)$ where v_0 is the vertical velocity of the particles on impact with the chute [m s⁻¹], L is the chute distance travelled [m], ω is the chute rotation speed [rad s⁻¹], μ is the shear friction factor, g is the acceleration of gravity [m s⁻²], and α is the angle of inclination of the chute compared to the axis of symmetry [rad]. Equations (2) and (3) describe the falling curve [1]. (2) $r(t) = L \sin \alpha + (v_1 \sin \alpha) t(2)$ (3) $y(t) = y_0 - L \cos \alpha - g t^2 / 2 - (v_1 \cos \alpha) t(3)$ After expressing time t from Equation (2) and substituting it into Equation (3) we get an Equation (4) of the falling curve. (4) $y = -g/2v_1^2 \sin^2 \alpha t^2 + gL - v_1 2 \cos \alpha v_1 \sin \alpha t + y_0 - gL/2v_1^2(4)$ where r represents the distance of the falling trajectory from the central axis, y is the vertical coordinate of the falling trajectory, v_0 is the vertical velocity of the particles on impact with the chute [m s⁻¹]. The L is the chute distance travelled [m], ω is the chute rotation speed [rad s⁻¹], μ is the shear friction factor, g is the acceleration of gravity [m s⁻²], α is the chute inclination angle compared to the axis of symmetry [rad], y_0 is the vertical coordinate of the beginning of the chute. Randomizing the velocity of the burden leaving the chute tip models the scatter of the charge on the impacting stockline surface. The volume of the charge falling into one annulus (a region bounded by two concentric circles) divides into virtual sub-charges with assigned various velocities for the scatter parameter. These sub-charges then move along various falling curves. This method brings the model closer to realistic conditions. The substitution by two or more lines, a cubic curve, or the Gaussian curve builds the burden profile mathematical model [2-5]. It is most often represented by two lines, which are beneath the material angles of repose and intersect on the falling trajectory [1, 6-8]. A polygonal chain gives the surface and interface between the burden components, which is composed of line segments passing through a sequence of points $P_i(r_i, y_i)$ called its vertices. Line Equation (5) describes the surface of the charge. (5) $p_i(r) = a_i r + b_i, i = 1, 2, \dots, n(5)$ In solving Equation (6), we find the intersection point of the falling curve with the polygonal chain representing the surface of the charge (including the furnace walls) determines the points of impact $I(r_i, y_i)$. (6) $0 = -g/2v_1^2 \sin^2 \alpha t^2 + gL - v_1 2(\cos \alpha - \mu \sin \alpha) v_1 \sin \alpha t + y_0 - gL/2v_1^2 - b_i(6)$ The maximum angle formed between the surface line of the cone formed by the charge and the horizontal plane represents the angle of repose. Generally, the repose angle depends on the properties of the material, like its density, size and grain shape, and the coefficient of friction of the material [9]. When the burden settles, its angle of repose varies concerning the axis of symmetry ϕ_{in} (inner angle) from the angle in the direction of the wall ϕ_{out} (outer angle). The repose angle in the direction of the wall is significantly smaller. Equations (7) and (8) express the nominal repose angles [8]. (7) $set_{in} = set_{max} C d^{0.054} F S^{0.05}(7)$ (8) $set_{out} = set_{in} R - r / 1.45(8)$ where set_{max} is the maximum angle of repose [deg], C is a constant, d is the diameter of the particle [m], FS is the shape dimensionless factor [-], R is the radius of the throat [m], r_i is the distance [m] from the symmetry axis to the intersection point of the trajectory and the burden surface. The falling trajectory, i.e. the chute angle, also affects the repose angle. In practice, angles of repose are determined experimentally with the help of scaled-down blast furnace models [8]. Then it is possible to connect individual repose angles with each position of the chute. Another option is to correct repose angles according to the deviation of the tangent angle $tl(r)$ to the falling trajectory at the point of impact. Equation (9) describes the tangent to the trajectory at the point of intersection. (9) $tl(r) = mlr + nl = -(grl - l \sin \alpha (v_0 \sin \alpha)^2 + \cot \alpha (\alpha)) r + (grl - l \sin \alpha (v_0 \sin \alpha)^2 - \cot \alpha (\alpha)) r_1 + y_l(9)$ (10) $ml = -(grl - l \sin \alpha (v_1 \sin \alpha)^2 - \cot \alpha (\alpha))(10)$ The slope of the ml tangent to the falling trajectory at the point of impact $tl(r)$ is used to determine the difference between the angle of incidence and the vertical axis, which is multiplied by the correction constants cin , $cout$ for a given type of angle. The resulting values are then subtracted from the nominal repose angles set_{in} , set_{out} . (11) $\phi_{in} = set_{in} + (n_2 + \tan - 1 ml) cin(11)$ (12) $\phi_{out} = (n_2 + \tan - 1 ml) cout - set_{out}(12)$ First, we must find the nearest point of the polygon chain of the charged surface (at the same or higher height) $P_j(r_j, y_j)$ to the intersection point $I(r_i, y_i)$. Depending on whether the found point is in the direction of the axis of symmetry or towards the charging system wall, a line $k(r)$ is run through the point under the inner ϕ_{in} or the outer repose angle ϕ_{out} . Subsequently, the algorithm inserts a line through the intersection point of this line $K(r_K, y_K)$ with the tangent to the trajectory $tl(r)$ under the second repose angle. (13) $k(r) = (\tan(\phi_{in})r + y_j - \tan(\phi_{in})r_j, r_j = r \tan(\phi_{in})r + y_K - \tan(\phi_{in})r_K, r_j = r(13)$ (14) $I(r) = (\tan(\phi_{out})r + y_j - \tan(\phi_{out})r_j, r_j > r(14)$ The intersection point of this second line with the polygon chain gives by the vertices $p_i(r_i)$ determines the second peripheral point of the surface of the added increment $L(r_L, y_L)$. The points $L(r_L, y_L)$, $K(r_K, y_K)$, $P_j(r_j, y_j)$ together with points $P_i(r_i, y_i), i = 1, 2, \dots, n$ that are not below the triangle L, K, P_j form a new surface resulting in the polygon chain containing the vertices $p(r)$. (15) $p(r) = \{a_i r + b_i, \min(r_L, r_j) < r < \max(r_L, r_j), i = 1, 2, \dots, nk(r), r \geq \min(r_L, r_j) \cup \min(r_L, r_j) \cup r$

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